то:	Erik Martin, PE, Sargent Engineers
FROM:	Calvin McCaughan, PE
DATE:	January 7, 2020
RE:	Summary of Geotechnical Engineering Services Chehalis Tribe Fish Hatchery Bridge Replacement Oakville, Washington

Introduction

This technical memorandum summarizes the results of geotechnical engineering services provided by Landau Associates, Inc. (LAI) in support of the Chehalis Tribe Fish Hatchery Bridge Replacement project. The project is located along Howanut Road in Oakville, Washington (site; Figure 1). Geotechnical services were provided in accordance with the scope outlined in the professional services agreement between LAI and Sargent Engineers, Inc. (Sargent, project civil engineer), authorized October 2, 2019.

Project Understanding

LAI's project understanding is based on information provided by representatives of Sargent and the Chehalis Indian Tribe (Chehalis Tribe, project owner) and on its review of available geologic and geotechnical documents regarding the site and the surrounding area.

The Chehalis Tribe proposes to replace a bridge along Howanut Road with a triple box culvert (three side-by-side culverts). Preliminary design drawings indicate that each culvert will have a 10-foot (ft)-wide by 8-ft-tall opening. The Chehalis Tribe used a similar culvert configuration in a recent project, and chose to use it here as well. Seismic design is not being considered.

Details regarding the triple box culvert and project earthwork are provided in Attachment 1. LAI understands that the finished roadway surface elevation, shown in Attachment 1, will approximate existing roadway grades.

Site Conditions

The site consists of a two-lane asphalt road, built on an embankment at the existing bridge crossing. The site is bordered by farmland to the south and by brush and blackberries to the north. The bridge crosses a seasonal flood channel that drains into Black River approximately 100 ft north of the site. The channel is partially lined with concrete, and riprap is present near its confluence with the river. Area residents have indicated that, historically, the channel has been used for cattle access.



During LAI's October 24, 2019 site visit, the channel was observed to be approximately 3 to 3.5 ft above the surface water elevation of Black River. The surface of Howanut Road is approximately 8.5 ft above the channel. These elevations are based on visual observations and measurements by LAI personnel. The channel was dry during LAI's site visit.

LAI's review of river hydrographs (Ecology 2019) indicates that, during its October 2019 site visit, the river stage was approximately 85.5 ft. (Here, river stage refers to the water level above the gauge at U.S. Highway 12, approximately 1 mile upstream of the site.) Review of historical hydrographs suggests that the river is typically 2 to 3 ft higher during the wet season (between November and April), and 1 ft lower in mid-summer.

Geologic Conditions

Geologic information for the site was obtained from the *Geologic Map of the Chehalis River and Westport Quadrangles, Washington* (Logan 1987). Vashon-age glacial outwash deposits are mapped at the site and in the surrounding area. The map identifies near-surface site soils as alluvium, a mixture of silt, sand, and gravel typically deposited in streambeds and fans. Vashon glacial outwash gravel consists of recessional and proglacial, stratified gravels, cobbles, and boulders deposited in meltwater streams and deltas. The glacial outwash gravel could contain ice-contact deposits and silt layers.

The subsurface conditions observed in LAI's explorations were generally consistent with the mapped geology.

Subsurface Conditions

Subsurface conditions were explored on October 24, 2019 by advancing and sampling two hollowstem auger borings (B-1 and B-2) at the approximate locations shown on Figure 2. Borings B-1 and B-2 were advanced 31.0 and 31.5 ft below ground surface (bgs), respectively.

Subsurface conditions were described using the soil classification system shown on Figure 3, in general accordance with ASTM International (ASTM) standard test method D2488, *Standard Practice for Description and Identification of Soils (Visual-Manual Procedures)*. Summary logs of the explorations are presented on Figures 4 and 5.

The soils observed underlying existing surface conditions (i.e., asphalt pavement) were categorized into three general units:

- **Fill:** Fill was observed in borings B-1 and B-2, and consisted of sandy gravel with silt in a medium dense, moist condition. The fill extended 5 to 6 ft bgs.
- Alluvium: Alluvium deposits were observed beneath the fill, and generally consisted of silt with sand in a soft, moist condition. The silt graded to loose, wet sand and gravel. The alluvium extended 18 to 20 ft bgs.

LAI interprets the upper portion (silt) of this unit to be moderately compressible. The moderately compressible soil extended to 15 ft bgs in boring B-1, and to 11 ft bgs in boring B-2.

• **Outwash:** Outwash deposits were observed beneath the alluvium, and consisted of sandy gravel with silt in a medium dense to very dense, wet condition. Both borings terminated in this unit.

During the October 2019 field investigation, groundwater was observed at 13 ft bgs, or approximately 1 ft below the river elevation at time of drilling. Site groundwater levels are likely to approximate the surface water elevation of Black River, and will vary depending on local subsurface conditions, weather conditions, and other factors. Furthermore, groundwater levels are expected to fluctuate seasonally, with maximum groundwater levels occurring between November and April.

Conclusions and Recommendations

Based on the conditions observed in LAI's subsurface explorations, shallow foundations should provide suitable support for the triple box culvert. The following key points should be considered during project planning and construction:

- Construction should be completed during the dry season (May to October). If construction is completed during the wet season, the proposed subgrade elevation could be submerged, and cofferdams and internal pumping may be required to complete dewatering.
- Excavating to the proposed subgrade elevation (approximately 13 ft bgs) is likely to expose areas of soft silt. Overexcavating these areas would expose the saturated, highly permeable soils underlying the silt. Rather than overexcavating, LAI recommends placing a geotextile at the base of the excavation. Vibratory compaction should not be used on the overlying bearing pad gravel.

Culvert Design

When preparing design recommendations, LAI assumed that backfill within the excavation zone (Attachment 1) would consist of Gravel Borrow conforming to the requirements in Section 9-03.14(1) of the Washington State Department of Transportation's 2018 Standard Specifications for Road, Bridge, and Municipal Construction (2018 WSDOT Standard Specifications). LAI also assumed that the Gravel Borrow would be compacted to at least 95 percent of its maximum dry density (MDD). The soil parameters provided in Table 1 can be used to design the replacement culvert.

Table 1. Culvert Wall Design Parameters

Devember	Value		
Parameter	Level Backslope		
Backfill soil unit weight (pcf)	125		
Backfill soil submerged unit weight (pcf)	63		
Backfill soil internal angle of friction (degrees)	34		
Foundation soil internal angle of friction (degrees)	30		
Active earth pressure coefficient (K _a)	0.28		
At-rest earth pressure coefficient (K ₀)	0.44		
Passive earth pressure coefficient (K_p)	3.54		
Ultimate coefficient of sliding	Cast-in-place: 0.57 Precast: 0.46		

Note: Wing walls typically are designed using active earth pressure, and box culvert walls using at-rest earth pressure. H = horizontal

pcf = pounds per cubic foot

V = vertical

Table 2 provides ultimate bearing resistances for strength, service, and extreme limit states for shallow foundation design.

Table 2. Nominal Bearing Resistance for Shallow Foundation Design

	Foundation Width (ft)	Ultimate Bearing Resistance (ksf)		
Foundation Type		Strength and Extreme Limit States	Service Limit State (2-inch Settlement)	
Closed Bottom Box Culvert	12	14.9	3.2	
Wing Wall Continuous Footing	8	12.3	4.0	

ft = feet

ksf = kips per square foot

Table 3 provides resistance factors for shallow foundation design (AASHTO 2017).

Table 3. Resistance Factors for Shallow Foundation Design

Limit State	Bearing	Sliding
Strength	0.45	Precast concrete: 0.90 Cast-in-place concrete: 0.80
Extreme	0.90	0.90
Service	1.0	1.0

Settlement Considerations

The 13-ft-deep structural excavation (including the bearing pad) will likely extend below the majority of compressible soil, and appreciable foundation settlement is not anticipated. However, 5 to 7 ft of compressible soil will remain in place beneath approach embankments. Approach embankments are likely to experience settlement if site grades are raised.

LAI estimates 1 to 2 inches of embankment settlement for every 1 ft that roadway grades are raised. Ninety percent of the total settlement should occur in the 6 months following construction. Localized pavement patching may be required within 5 years of construction.

Construction Considerations

The following geotechnical recommendations should be considered during preparation of project specifications:

- **Temporary excavations:** Temporary excavations should be completed in accordance with the guidelines set forth in Section 2-09 of the *2018 WSDOT Standard Specifications*. The contractor should be responsible for actual trench configurations and the maintenance of safe working conditions. Temporary excavations in excess of 4 ft should be shored or sloped in accordance with the requirements outlined in Safety Standards for Construction Work, Part N (Washington State Department of Labor and Industries, Chapter 296-155 of the Washington Administrative Code). The material likely to be exposed in the structural excavations should be considered Type C soil with a maximum allowable excavation inclination of 1.5 horizontal to 1 vertical (1.5H:1V).
- **Dewatering:** During LAI's October 2019 field investigation, groundwater was observed at 13 ft bgs. At that time, the surface water elevation of nearby Black River was estimated at 12 ft bgs. A 13-ft-deep excavation is proposed for the replacement structure. As such, the excavation may be constructed below groundwater. (Note: The seasonal high groundwater table is estimated to be a few feet more than the observed groundwater elevation, and the seasonal low groundwater table is estimated to be approximately 1 ft less.)

Soils observed beneath the silt layer (designated "ML" on Figures 4 and 5) are granular and readily transmit groundwater. In LAI's experience, a 13-ft-deep excavation that is left open for more than a few hours will flood, producing groundwater levels equal to nearby surface water levels.

If excavation into groundwater (below river level) is required, conventional sumps and pumps are unlikely to provide a dry, stable work area. Installation of shallow cofferdams and trash pumps should be anticipated. Completing construction between May and October will reduce dewatering needs. The contractor should be responsible for design and implementation of the dewatering system.

• Sheet pile shoring systems: Depending on the construction schedule, installation of sheet pile shoring systems/cutoff walls may be required. The parameters provided in Table 4 can be used to design engineered shoring systems, if needed. Given the density of outwash soil deposits, it may be difficult to install sheet piles more than 20 ft bgs.

Soil Unit	Moist Unit Weight (pcf)	Submerged Unit Weight (pcf)	Cohesion (psf)	Internal Angle of Friction (degrees)
Fill	125	62	0	34
Alluvium	110	48	0	30
Outwash	_	62	0	38

Table 4. Recommended Soil Parameters for Design of Temporary Shoring

pcf = pounds per cubic foot

psf = pounds per square foot

- **Subgrade preparation:** The prepared subgrade should be evaluated by a qualified civil or geotechnical engineer, who is familiar with the site and can check for soft and/or disturbed areas. To help stabilize soft, inorganic materials, a non-woven geotextile should be placed along the base of the excavation, per Section 9-33.2(1), Table 3 of the 2018 WSDOT Standard Specifications.
- **Reuse of site soil:** Site soils may contain creosote from structural remnants (Figure 5), and reuse should be coordinated with the Chehalis Tribe. If clean of hazardous materials, fill soils within the top 5 ft of the existing grade (designated "GP-GM" on Figures 5 and 6) can be reused as structural fill during dry weather. Other site soils have a high fines and moisture content, and are not suitable for reuse as structural fill.
- Import structural fill: Gravel Borrow, conforming to the requirements in Section 9-03.14(1) of the 2018 WSDOT Standard Specifications, is a suitable source of import structural fill. During periods of wet weather, the fines content should not exceed 5 percent, based on the minus ¾- inch fraction. Import structural fill should be used as backfill within the limits of the structural excavation.
- **Backfilling:** Backfill around structures should be placed and compacted in accordance with Section 2-03.3(14)C, Method C of the 2018 WSDOT Standard Specifications. Compaction and moisture control tests should be performed in accordance with Section 2-03.3(14)D of the 2018 WSDOT Standard Specifications. Alternatively, the MDD and optimum moisture content can be determined using ASTM standard test method D1557.
- **Roadway embankments:** If widened, roadway embankments should have side slopes of 2H:1V or flatter, in accordance with Section 2-03 of the *2018 WSDOT Standard Specifications*.
- **Pavement design:** In-kind pavement sections are anticipated.

Plan Review Notes

The earthwork notes in the current project plans (Attachment 1) are generally consistent with LAI's geotechnical recommendations. The following material specifications align with LAI's understanding of proposed earthwork, and can be added to the plans, if needed:

• Backfill within structural excavation limits: Gravel Borrow, as described in Section 9-03.14(1) of the 2018 WSDOT Standard Specifications.

- Gravel Base: Ballast, as described in Section 9-03.9(1) of the 2018 WSDOT Standard Specifications.
- General fill to raise site grades or to be placed outside of the structural excavation limits: Select Borrow, as described in Section 9-03.14(2) of the 2018 WSDOT Standard Specifications.
- Crushed Surfacing Top Course: Section 9-03.9(3) of the 2018 WSDOT Standard Specifications.
- Class A Rock for Erosion Protection: Section 9-13.4(2) of the 2018 WSDOT Standard Specifications.
- Geotextile beneath box culverts: Section 9-33.2(1) of the 2018 WSDOT Standard Specifications, Table 3, for Soil Stabilization, Non-Woven. LAI suggests adding this element to the plan sheets.
- Geotextile for permanent erosion control: Section 9-33.2(1) of the 2018 WSDOT Standard Specifications, Table 4, Permanent Erosion Control, Moderate Survivability, Non-Woven.

Use of This Technical Memorandum

This technical memorandum has been prepared for the exclusive use of Sargent Engineers, Inc. and the Chehalis Indian Tribe for specific application to the Chehalis Tribe Fish Hatchery Bridge Replacement project in Oakville, Washington. Use of the information contained in this technical memorandum by others or for another project is at the user's sole risk. The findings, recommendations, and opinions presented herein are based on the field investigation completed for the project.

Closing

We trust that this memorandum provides you with sufficient information to proceed with the project. If you have questions or comments, or if we may be of further service, please contact the undersigned at (360) 791-3178.

LANDAU ASSOCIATES, INC.

Calvin McCaughan, PE Principal

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Attachments: Figure 1. Vicinity Map Figure 2. Site and Exploration Location Plan Figure 3. Soil Classification System and Key Figures 4 and 5. Logs of Borings B-1 and B-2 Attachment 1. Box Culvert Sections/Details



Summary of Geotechnical Engineering Services Chehalis Tribe Fish Hatchery Bridge Replacement

References

- AASHTO. 2017. *Load and Resistance Factor Design Bridge Design Specifications, Customary U.S. Units.* 8th Edition. American Association of State Highway and Transportation Officials. September.
- ASTM. 2017. Annual Book of ASTM Standards. In: Soil and Rock(I). West Conshohocken, PA. ASTM International.
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- Logan, R.L. 1987. *Geologic Map of the Chehalis River and Westport Quadrangles, Washington.* Washington State Department of Natural Resources.
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- WSDOT. 2017. *M41-10: Standard Specifications for Road, Bridge, and Municipal Construction 2018.* Washington State Department of Transportation. December 1.



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Soil Classification System						
	MAJOR DIVISIONS		GRAPHI SYMBO	L SYMBOL ⁽¹⁾		
	GRAVEL AND	CLEAN GRAVEL	00000	GW	Well-graded gravel; gravel/sand mixture(s); little or no fines	
SOIL ial is size)	GRAVELLY SOIL	(Little or no fines)	00000	o GP	Poorly graded gravel; gravel/sand mixture(s); little or no fines	
ED S nateri	(More than 50% of	GRAVEL WITH FINES	EBEEE	GM	Silty gravel; gravel/sand/silt mixture(s)	
AINE	on No. 4 sieve)	(Appreciable amount of fines)	1]]]	GC	Clayey gravel; gravel/sand/clay mixture(s)	
50% 50%	SAND AND	CLEAN SAND		SW	Well-graded sand; gravelly sand; little or no fines	
SSE- than than	SANDY SOIL	(Little or no fines)		SP	Poorly graded sand; gravelly sand; little or no fines	
OAF Aore rger 1	(More than 50% of	SAND WITH FINES		SM	Silty sand; sand/silt mixture(s)	
0 <i>∈</i> <u></u>	through No. 4 sieve)	(Appreciable amount of fines)		SC	Clayey sand; sand/clay mixture(s)	
) an UL	SILTA			ML	Inorganic silt and very fine sand; rock flour; silty or clayey fine sand or clayey silt with slight plasticity	
0 SC % of er th size)				CL	Inorganic clay of low to medium plasticity; gravelly clay; sandy clay; silty clay; lean clay	
n 50 mall ieve	Liquid lim	it less than 50)		OL	Organic silt; organic, silty clay of low plasticity	
e tha e tha al is s 200 s				MH	Inorganic silt; micaceous or diatomaceous fine sand	
Mor Mor No. 2				СН	Inorganic clay of high plasticity; fat clay	
Z Ĕ	Liquid limit	greater than 50)		OH	Organic clay of medium to high plasticity; organic silt	
	HIGHLY O	RGANIC SOIL		PT	Peat; humus; swamp soil with high organic content	
	OTHER MATERIALS			C LETTER	TYPICAL DESCRIPTIONS	
	PAVEM	ENT	•	AC or PC	Asphalt concrete pavement or Portland cement pavement	
	ROC	К		RK	Rock (See Rock Classification)	
	WOO	D		WD	Wood, lumber, wood chips	
	DEBR	IS	6/0/0	DB	Construction debris, garbage	
 (e.g., SP-SM for salid of gravely indicate soft with an estimated S-15% lines. Multiple letter symbols (e.g., MDOL) indicate boldenine of multiple soft classifications. Soil descriptions are based on the general approach presented in the Standard Practice for Description and Identification of Soils (Visual-Manual Procedure), outlined in ASTM D 2488. Where laboratory index testing has been conducted, soil classifications are based on the Standard Test Method for Classification of Soils for Engineering Purposes, as outlined in ASTM D 2487. Soil description terminology is based on visual estimates (in the absence of laboratory test data) of the percentages of each soil type and is defined as follows: Primary Constituent: > 50% - "GRAVEL," "SAND," "SILT," "CLAY," etc. Secondary Constituents: > 30% and ≤ 50% - "very gravelly," "very sandy," "very silty," etc. > 15% and ≤ 30% - "gravelly," "sandy," "silty," etc. Additional Constituents: > 5% and ≤ 15% - "with gravel," "with sand," "with silt," etc. ≤ 5% - "with trace gravel," "with sand," "with race silt," etc., or not noted. Soil density or consistency descriptions are based on judgement using a combination of sampler penetration blow counts, drilling or excavating 						
	Drilling	and Sampling Ke	Ŵ		Field and Lab Test Data	
	SAMPLER TYPE	SAMPLE	NUMBER 8	& INTERVAL		
Code Description a 3.25-inch O.D., 2.42-inch I.D. Split Spoon b 2.00-inch O.D., 1.50-inch I.D. Split Spoon c Shelby Tube d Grab Sample			Sample Ider	tification Number	Code Description PP = 1.0 Pocket Penetrometer, tsf TV = 0.5 Torvane, tsf PID = 100 Photoionization Detector VOC screening, ppm W = 10 Moisture Content, % D = 120 Dury Density, pcf	-
f Double-Tube Core Barrel g 2.50-inch O.D., 2.00-inch I.D. WSDOT h 3.00-inch O.D., 2.375-inch I.D. Mod. California i Other - See text if applicable 1 300-lb Hammer, 30-inch Drop 2 140-lb Hammer 30-inch Drop			- Portion of for A	ple Depth Interval Sample Retained rchive or Analysis	-200 = 60 Material smaller than No. 200 sieve, % GS Grain Size - See separate figure for data AL Atterberg Limits - See separate figure for data GT Other Geotechnical Testing CA Chemical Analysis	
3 Pushed GIOUIIUWaleI				of drilling (ATD)	\neg	
5 Othe	er - See text if applicable		proximate w	ater level at time a	after drilling/excavation/well	
LANDAU ASSOCIATES Chehalis Tribe Fish Hatchery Bridge Replacement Oakville, Washington Soil Classification System and Key					assification System and Key 3	re





ATTACHMENT 1

Box Culvert Sections/Details

- GROUT. JOINT SEALANT AND PRIMERS SHALL BE INCLUDED IN THE COST PER LINEAR FOOT OF BOX CULVERT.

- PREPARATION. BACKFILLING OF THE TRENCH SHOULD BE FILLED TO THE LEVEL OF THE TOP OF THE CULVERT, FILLING AND COMPACTING EVENLY ON EACH SIDE.



